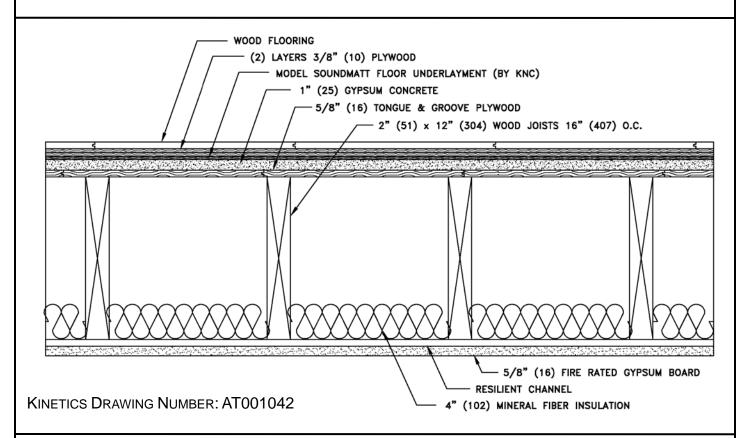
KINETICS NOISE CONTROL TEST REPORT #AT001042

- KINETICS NOISE CONTROL PRODUCTS:
 - SOUNDMATT
- ACOUSTICAL RATINGS:
 - o STC 58
 - o IIC 54
- TESTING AGENCY & REPORT NUMBER:
 - National Research Council of Canada
 - o B-3463.10





6300 IRELAN PLACE, DUBLIN OH PHONE: 800.959.1229 FAX: 614.889.0540

WEB: <u>www.KineticsNoise.com</u> Email: <u>ArchSales@KinetisNoise.com</u> National Research Council of Canad Client Report
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Airborne Sound Transmission Loss and the Impact Sound Transmission Measurements Performed on One Floor Assembly for Kinetics Noise Control

for

Kinetics Noise Control 6300 Ireland Place Dublin, Ohio 43017-0655 USA Airborne Sound Transmission Loss and Impact Sound Transmission Measurements Performed on One Floor Assembly for Kinetics Noise Control

Author

N.L. Brunette

Quality Assurance

J.D. Quirt, Ph.D.

Group Leader

Approved

M.R. Atif, Ph.D.

Director, Indoor Environment

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INTRODUCTION

SPECIMEN DESCRIPTION

Airborne and impact sound transmission measurements were performed on one floor assembly. For report purposes, the floor is identified as Floor "A". Please note that this floor assembly was tested under contract B3103, but an individual report for this specimen was not requested or issued as part of that contract.

Construction on the series of floor assemblies for this contract started in August, 1997 and concluded in October 1997. The airborne and impact sound transmission loss tests for this floor assembly were performed on August 28th, 1997.

Floor "A"

The 38 mm x 292 mm solid wood joists were spaced 406 mm on center. The USG RC1 resilient channels were installed perpendicular to the wood joists and spaced 610 mm on center. The single layer of gypsum board was installed with the long edge of sheets perpendicular to the resilient channels. The gypsum board was attached with 32 mm gypsum board screws spaced 305 mm on center.

USG Thermafibre batts were installed in the joist cavities. Cotton string was stapled 50 mm from the bottom of each joist cavity, every 406 mm, perpendicular to the joists to ensure that the insulation did not touch the gypsum board.

The single layer of 16 mm tongue and groove plywood was installed perpendicular to the wood joists and was attached using 25 mm wood screws spaced 305 mm on center. The 15 lb. roofing felt was laid on top of the 16 mm plywood. The joints of the strips of roofing felt overlapped by 50 mm.

On August 21, 1997, a layer of 25 mm thick Dura-Cap gypsum concrete was poured on top of the roofing felt. The Dura-Cap was installed according to the manufacturer's instructions. Two layers of sill gasket were used around the perimeter to isolate the Dura-Cap slab from the test frame. Once the Dura-Cap had cured according to the manufacturer's instructions, sheets of Soundmatt were laid on top of the Dura-Cap. The edges of the Soundmatt sheets were butted together. The base layer of 9.5 mm plywood was laid directly on top of the Soundmatt. The face layer of 9.5 mm plywood was glued to the base layer and screwed with 16 mm wood screws in the corners of each sheet and 305 mm on center. The face layer of plywood was installed perpendicular to the base layer. The parquet flooring was

glued to the face layer of plywood as per the manufacturer's instructions.

The following table gives the elements of the specimen, listed from top to bottom.

Table 1: Element breakdown of Floor "A".

Element	Surface weight (kg/m²)	Mass (kg)
8 mm parquet flooring	5.7	113.9
9.5 mm plywood	4.1	82.1
9.5 mm plywood	3.9	78.7
8 mm Soundmatt	1.0	19.6
25 mm "Dura-Cap" gypsum concrete	47.3	946.0
roofing felt	0.4	9.5
16 mm tongue and groove plywood	6.6	133.0
292 mm wood joists, 406 mm o.c.		271.5
102 mm mineral fiber batts	7.6	131.0
13 mm RC1 resilient channels, 610 mm o.c.		7.6
15.9 mm fire-rated gypsum board	11.1	199.2
TOTAL		1992.1

Total thickness: 397 mm

The test specimen was mounted in the IRC acoustical floor test opening which measures $4.70 \text{ m} \times 3.78 \text{ m}$. The area used for the calculations of impact transmission and airborne sound transmission loss was 17.85 m^2 .

RESULTS

Results of the airborne sound transmission loss measurements of Floor "A" are given in Table 2 and Figure 1. Results of the impact sound transmission measurements of this floor construction are given in Table 3 and Figure 2.

Values marked "c" indicate that at these frequencies, the measured background level was between 5 dB and 10 dB below the combined receiving room level and background level. The reported values have been corrected for the influence of background noise and provide an estimate of the lower limit of airborne sound transmission loss. These values do not limit the sound transmission class unless otherwise indicated.

Values marked "*" indicate that the measured background level was less than 5 dB below the combined receiving room level and background level. The reported values provide an estimate of the lower limit of airborne sound transmission loss or impact transmission. These values do not limit the sound transmission class.

The Tables also give the 95% confidence limits. Acoustical measurement in rooms is a sampling process and as such has associated with it a degree of uncertainty. By using enough microphone and loudspeaker positions, the uncertainty can be reduced and upper and lower limits assigned to the probable error in the measurement. These limits are called 95% confidence limits. They are calculated for each test according to the procedures in ASTM E90 and E492 and must be less than upper limits given in the standards. These confidence limits do not relate directly to the variation expected when a nominally identical specimen is built, installed and tested (repeatability). Nor do they relate to the differences expected when nominally identical specimens are tested in different laboratories (reproducibility).

Table 2: Airborne sound transmission loss measurements of Floor "A", TLF-97-077/078.

Frequency (Hz)	Airborne Sound Transmission Loss (dB)	95% Confidence Limits*	Deviation Below the STC Contour	
80	34	±3.1		
100	38	±2.0		
125	39	±1.5	3	
160	37	±1.0	8	
200	45	±1.1	3	
250	56	±0.6		
315	64	±0.5		
400	72	±0.4		
500	78	±0.6		
630	83	±0.4		
800	88c	±0.4		
1000	91c	±0.4		
1250	92c	±0.3		
1600	93	±0.5		
2000	92	±0.4		
2500	92	±0.5		
3150	96	±0.4		
4000	99	±0.3		
5000	101	±0.5		
Sound Transmission Class (STC) ¹ = 58				

Weighted Sound Reduction $(R_W)^2 = 62$

¹ Sound Transmission Class (STC) calculated according to ASTM E413.

 $^{^{2}}$ Weighted Sound Reduction (R $_{\!\scriptscriptstyle W}\!)$ calculated according to ISO 717.

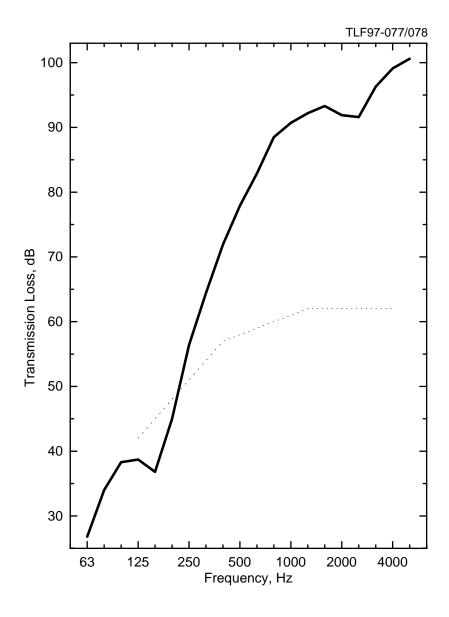


Figure 1: Airborne sound transmission loss measurements of Floor "A". The solid line is the experimental data, the dotted line is the STC 58.

Table 3: Impact sound transmission measurements of Floor "A", IIF-97-038.

Frequency (Hz)	Impact Sound Transmission Loss (dB)	95% Confidence Limits*	Deviation Below the IIC Contour		
80	64	±1.0			
100	61	±0.7	3		
125	63	±0.6	5		
160	66	±0.5	8		
200	61	±0.3	3		
250	56	±0.2			
315	53	±0.2			
400	45	±0.2			
500	39	±0.2			
630	32	±0.1			
800	27	±0.1			
1000	24	±0.1			
1250	21	±0.2			
1600	17	±0.3			
2000	18c	±0.4			
2500	18c	±0.7			
3150	21*	±2.1			
4000	21*	±2.2			
5000	18*	±1.4			
Impact Inculation Class (IIC) ³ F4					

Impact Insulation Class $(IIC)^3 = 54$

Weighted Normalized Impact Sound Pressure Level $(L_{n,w})^4 = 53$

³ Impact Insulation Class (IIC) calculated according to ASTM E989.

 $^{^{\}scriptscriptstyle 4}$ Weighted Normalized Impact Sound Pressure Level (Ln,w) calculated according to ISO 717.

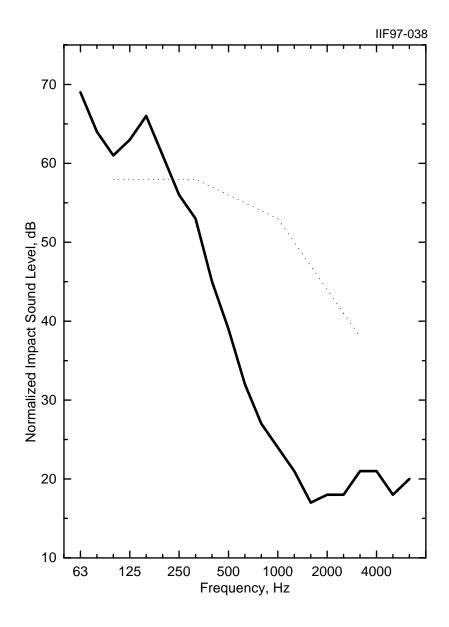


Figure 2: Impact sound transmission measurements of Floor "A". The solid line is the experimental data and the dotted line is the IIC 54 contour.

NOTES ON THE SIGNIFICANCE OF TEST RESULTS

Sound Transmission Class And Weighted Sound Reduction Index

The Sound Transmission Class (STC) and Weighted Sound Reduction Index (R_w) are single-figure rating schemes intended to rate the acoustical performance of a partition element under typical conditions involving office or dwelling separation. The higher the value of either rating, the better the floor performance. Thus, the rating is intended to correlate with subjective impressions of the sound insulation provided against the sounds of speech, radio, television, music, office machines and similar sources of noise characteristic of offices and dwellings. In applications involving noise spectra that differ markedly from those referred to above (for example, heavy machinery, power transformers, aircraft noise, motor vehicle noise), the STC and R_w are of limited use. Generally, in such applications it is desirable to consider explicitly the noise spectra and the insulation requirements.

Impact Insulation Class And Weighted Normalized Impact Sound Pressure Level

The Impact Insulation Class (IIC) (ASTM E989) and the Weighted Normalized Impact Sound Pressure Level ($L_{n,w}$) (ISO 717-2) are single-figure rating schemes intended to rate the effectiveness of floor-ceiling assemblies at preventing the transmission of impact sound from the standard tapping machine. The higher the value of the rating, the better the floor performance.

The ASTM E989 and the ISO 717 rating curves are identical. The major difference in the fitting procedure is that the ISO standard allows unfavorable deviations to exceed 8 dB; the ASTM E989 standard does not. When this 8 dB requirement is not invoked, the two ratings are related by the equation

 $IIC = 110 - L_{n.w}$

Extended Frequency Range

Standard test procedures require measurements in 1/3-octave bands over a specified frequency range (125 to 4000 Hz for ASTM E90 and 100 to 3150 Hz for ASTM E492). Within those ranges, reproducibility has been assessed by inter-laboratory round robin studies. The standards recommend making measurements and reporting results over a larger frequency range, and this report presents such

results, which may be useful for expert evaluation of the specimen performance. The precision of results outside the standard ranges has not been established, and is expected to depend on laboratory-specific factors such as room size and specimen dimensions.

FACILITIES AND EQUIPMENT

The acoustics floor test facility comprises two reverberation rooms with a moveable test frame between the two rooms. Both rooms have a volume of 175 m³.

Measurements are controlled by a desktop PC-type computer interfaced to a Norwegian Electronics type 830 real time analyser. Each room has a calibrated Bruel & Kjaer condenser microphone with a type 4166 cartridge that is moved under computer control to nine positions used for the acoustical measurements. Each room has four loudspeakers driven by separate amplifiers and noise sources. To increase the randomness of the sound field, there are also fixed diffusing panels in each room.

TEST PROCEDURE

Airborne Sound Transmission Loss

Airborne sound transmission measurements were conducted in accordance with the requirements of ASTM E90, "Standard Method for Laboratory Measurement of Airborne Sound Transmission Loss of Building Partitions", and of ISO 140-3, "Laboratory Measurement of Airborne Sound Insulation of Building Elements".

The Sound Transmission Class (STC) was determined in accordance with ASTM E413, "Classification for Rating Sound Insulation". The Weighted Sound Reduction Index (R_w) was determined in accordance with ISO 717-1, "Rating of Sound Insulation in Buildings and of Building Elements, Part 1: Airborne Sound Insulation".

One-third octave band sound pressure levels were measured for 30 seconds at each microphone position in each room and then averaged to get the average sound pressure level in the room. Five sound decays were averaged to get the reverberation time at each microphone position in the receiving room. These times were averaged to get the average reverberation times for the room.

The average sound pressure levels of both the source and receiving rooms and the average reverberation times of the receiving room were used to calculate sound transmission loss values.

Airborne sound transmission loss tests were performed in the forward (receiving room is the lower room) and reverse (receiving room is the upper room) directions. Results presented in this report are the average of the tests in these two directions.

A complete description of the test procedure, information on the flanking limit of the facility and reference specimen test results are available on request.

Impact Sound Transmission

Impact sound transmission measurements were made in accordance with ASTM E492, "Standard Test Method for Laboratory Measurement of Impact Sound Transmission Through Floor-Ceiling Assemblies Using the Tapping Machine". This test used the standard tapping machine and the prescribed four impact positions on the floor. The Impact Insulation Class (IIC) was determined in accordance with ASTM E989, "Standard Classification for Determination of Impact Insulation Class (IIC)".

These measurements are also in accordance with ISO 140-6, "Laboratory Measurements of Impact Sound Insulation of Floors", except that the tapping machine positions are not randomly selected. This difference is believed to be insignificant. The Weighted Normalized Impact Sound Pressure Level ($L_{n,w}$) was determined in accordance with ISO 717-2, "Acoustics — Rating of Sound Insulation in Buildings and of Building Elements - Part 2: Impact Sound Insulation".

One-third octave band sound pressure levels were measured for 30 seconds at each microphone position in the receiving room and then averaged to get the average sound pressure level in the room. Five sound decays were averaged to get the reverberation time at each microphone position in the receiving room. These times were averaged to get the spatial average reverberation times for the room.

The space average sound pressure levels and the spatial average reverberation times of the receiving room were used to calculate impact transmission values. For impact sound transmission, the lower room is the receiving room.

A complete description of the test procedure is available on request.

Special Impact Test (Tire, Walker, Ball)

There is no standard test specifying how to measure the sound pressure levels generated by a person walking on a floor. Several years ago in ASTM committee E33, a single microphone measurement technique was proposed and was adopted for use in this laboratory. A single microphone is placed 1 m below the mid-point of the ceiling and the room below is made much less reverberant by placing sound absorbing material in it. The same microphone technique is used for measuring walker, ball and tire levels.

The Japanese measurement standard JIS 1418 specifies a heavy impactor source for evaluating floor constructions. It consists of an automobile tire mounted on an arm attached to motor. The motor lifts the tire and then utilizes cams to drop the tire freely on the floor. The cam system prevents the tire from striking the floor again until it has been lifted to the correct drop height. JIS 1418 specifies many drop positions for the tire and several microphone positions. Earlier research with this machine showed that only a few positions of the tire were necessary. The single microphone position is also considered adequate for comparison of floors tested within a single laboratory.

For the walker tests, a male member of the laboratory walks for about 3 minutes while the computer collects maximum sound levels for each 100 footsteps using a 35 ms time constant.

The ball used in these measurements was developed by H. Tachibana as part of his research. The ball is 180 mm in diameter and weighs 2.5 kg. It is dropped from a height of 900 mm. The force generated is sufficiently repeatable that only 15 impulses need be averaged.